



Combined amperometric/field-effect sensor for the detection of dissolved hydrogen

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ABSTRACT

Real-time and reliable monitoring of the biogas process is crucial for a stable and efficient operation of biogas production in order to avoid digester breakdowns. The concentration of dissolved hydrogen (H_2) represents one of the key parameters for biogas process control. In this work, a one-chip integrated combined amperometric/field-effect sensor for monitoring the dissolved H_2 concentration has been developed for biogas applications. The combination of two different transducer principles might allow a more accurate and reliable measurement of dissolved H_2 as an early warning indicator of digester failures. The feasibility of the approach has been demonstrated by simultaneous amperometric/field-effect measurements of dissolved H_2 concentrations in electrolyte solutions. Both, the amperometric and the field-effect transducer show a linear response behaviour in the H_2 concentration range from 0.1 to 3% (v/v) with a slope of 198.4 ± 13.7 nA/% (v/v) and 14.9 ± 0.5 mV/% (v/v), respectively.

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1. Introduction

A stable and efficient operation of the biogas production has the potential to replace some of the limited fossil fuels [1]. The use of biogas as energy source is currently establishing in the group of alternative energies. In general, the natural process of anaerobic digestion is a relative stable system that occurs in nature without the need for precise process control. However, under high loading conditions, process failures such as disadvantageous biogas yield or stoppage of the biogas production due to acidification of the medium are known to occur [2–4]. Therefore, real-time and reliable controlling and monitoring of the biogas process is crucial for a stable and efficient operation of biogas production in order to avoid digester breakdowns.

The concentration of dissolved hydrogen (H_2) represents one of the most important parameters for biogas process control in anaerobic digesters [5,6]. Accumulated H_2 strongly inhibits the degradation of volatile fatty acids, such as propionate and butyrate, resulting in a consequent deterioration of normal operation [7]. A build-up of hydrogen above a critical concentration of higher than $0.04 \mu\text{M}$ has been reported as initial stage of digester overload-ing [7,8]. If hydrogen production exceeds the maximum ability of

the methanogenic biomass to degrade hydrogen, there will be a rapid and large increase in the hydrogen concentration prior to digester failures. Thus, dissolved hydrogen is a key factor in the intricate balance between microbial species involved in the multi-step degradation during anaerobic digestion, making it a useful parameter for biogas process monitoring and early warning of process disturbances [2,3,9–12].

Most of hydrogen sensors, used for monitoring the anaerobic biogas production, are based on the detection of H_2 in the gas phase of the digester [5,13–15]. Dissolved H_2 in the liquid medium is thus calculated from the gas fraction, assuming that the hydrogen-transfer rate between the gas and the liquid phase is not limited. However, H_2 mass-transfer coefficients in anaerobic digesters are much smaller than those typically found in aerobic fermentation digesters [16]. That is because the culture broth of anaerobic digestion consists of a complex physico-chemical composition with respect to the H_2 solubility [17,18]. This limits the rapidity with which an increase in H_2 concentration in the biomass can be detected in the gas phase of the digester. As a consequence, serious overloading of the digester may occur before the raised H_2 concentration in the gas phase is detected. Therefore, having a practical, reliable and low-cost instrumentation that provides a continuous and in situ measurement of dissolved hydrogen in anaerobic digesters would be highly advantageous.

In this work, a Si-based combined chemosensor capable for the simultaneous amperometric/field-effect detection of the concentration of dissolved H_2 has been developed for biogas applications. Such a combination of two different transducer principles for

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the detection of the same parameter might allow a more accurate, selective and reliable measurement of dissolved H_2 as an early warning indicator of digester failures. The functioning of the developed one-chip integrated dual amperometric/field-effect chemosensor has been tested in electrolyte solutions with different concentrations of dissolved H_2 .

2. Experimental

2.1. Structure and functioning principle of the combined H_2 sensor

The schematic layer structure of the combined dissolved H_2 sensor and the measurement set-up for the simultaneous amperometric/field-effect detection of dissolved H_2 in electrolyte solutions is shown in Fig. 1. The developed sensor combines a pH-sensitive capacitive EIS (electrolyte-insulator-semiconductor) sensor consisting of an Al–p-Si–SiO₂–Ta₂O₅ structure and two circular-type thin-film Pt electrodes. The specific feature of the combined H_2 -sensor chip is the implementation of the field-effect pH sensor in addition to well-known amperometric measurements. The field-effect pH sensor is a basic structural element of current chemical sensors and biosensors [19–25] and is used in this approach for an indirect detection of the dissolved H_2 gas. This new approach has been introduced by the authors for the first time in [26]. Thus, two transduction principles are closely combined at the microscale, enabling new electrochemical detection opportunities.

The operation principle of the combined sensor structure is assumed to be as follows. Dissolved H_2 diffuses to the polarized Pt working electrode and is electrochemically oxidized according to the following reaction [27,28]:



This causes a current depending on the dissolved hydrogen concentration. If the potential of the working electrode is adjusted (usually +0.55 V vs. Ag/AgCl reference electrode) that any hydrogen molecule reaching the electrode surface is immediately oxidized, then the current will be controlled solely by the diffusion rate of hydrogen to the electrode surface. The most important difference of our H_2 -sensor chip and other macro- or miniaturized

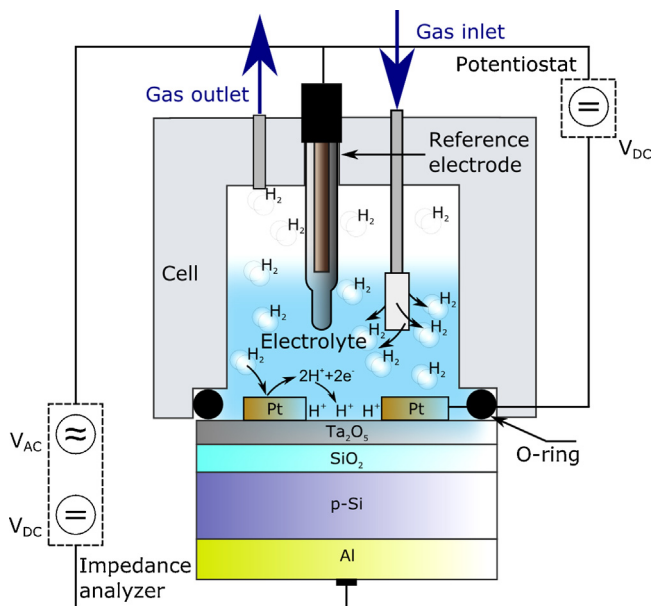


Fig. 1. Schematic structure and measurement set-up of the combined amperometric/field-effect dissolved H_2 sensor.

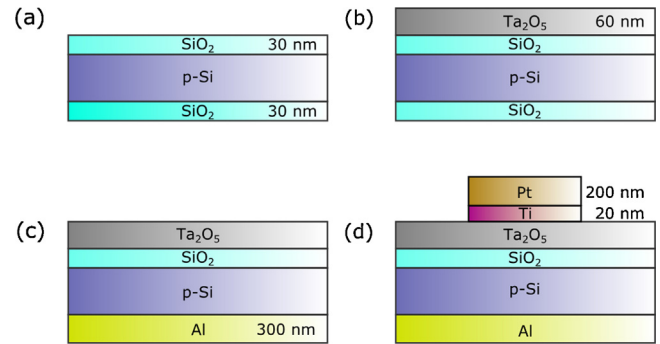


Fig. 2. Flowchart for the fabrication of the combined dissolved H_2 sensor: (a) p-Si wafer with thermally grown SiO₂; (b) deposition of tantalum and thermal oxidation to Ta₂O₅; (c) etching of SiO₂ on the rear side and deposition of the Al back-side contact; (d) deposition and patterning of the circular Pt thin-film electrodes.

amperometric H_2 sensors reported in literature [15,27,29,30], is the existence of the one-chip integrated field-effect sensor, capable for an indirect detection of dissolved H_2 . The product of H_2 oxidation, i.e., H^+ ions generated at the working electrode (see Eq. (1)), will diffuse to the pH-sensitive gate-insulator surface (in this study, Ta₂O₅) and will be detected there. A resulting local pH decrease near the surface of the pH-sensitive layer leads to a change in the surface charge and thus, modulates the space-charge capacitance in the Si and consequently, the flatband voltage and capacitance of the EIS structure. In previous experiments, field-effect devices have been successfully used for the detection of H^+ ions that have been electrochemically generated via electrolysis of water [31,32]. The output signal of the combined sensor is considered as “ H_2 signal” only, if the signal changes of both the amperometric and the field-effect sensor are nearly simultaneous (with a small delay time necessary for the diffusion of H^+ ions generated at the amperometric electrode to the gate region of the field-effect sensor) and if the signal of the field-effect sensor is shifted towards more negative potentials that corresponds to an increase of the H^+ concentration. In this way, the selectivity of the combined sensor to H_2 detection can be achieved.

2.2. Fabrication of the combined sensor structure

The flowchart for the fabrication of the combined amperometric/field-effect H_2 sensor is shown in Fig. 2. For the realization of the field-effect sensor, capacitive Al–Si–SiO₂–Ta₂O₅ (p-Si, $\rho = 1\text{--}10\ \Omega\text{cm}$; 30 nm thermally grown SiO₂ (Fig. 2a)) structures with a Ta₂O₅ layer as pH-sensitive gate insulator material have been fabricated. Ta₂O₅ is widely used for field-effect pH sensing, due to its high pH sensitivity [33] as well as high corrosion-resistance properties in a wide pH range [34]. The Ta₂O₅ films were prepared by means of thermal oxidation of an electron-beam deposited, 30 nm thick tantalum layer in dry oxygen atmosphere at 517 °C for about 30 min, yielding a ~60 nm thick Ta₂O₅ layer (Fig. 2b). After etching the SiO₂ from the rear side of the wafer, a 300 nm Al film was deposited as a contact layer for the field-effect sensor (Fig. 2c).

For the preparation of the amperometric transducer, a Pt layer with a thickness of 200 nm was deposited together with an adhesion layer of 20 nm Ti by means of electron-beam evaporation and patterned as circular electrodes via photolithography and lift-off technique, respectively (see Fig. 2d). Platinum has an excellent electro-catalytic activity for hydrogen oxidation as compared to other metals [35,36]. In a following step, the wafer was separated into single sensor chips with a size of 10 mm × 14 mm and assembled onto a printed circuit board (PCB). For electrical connection of the field-effect sensor, the Al rear-side contact of the EIS structure was glued with electrically conductive adhesive onto the PCB

substrate. The front-side contacts to the platinum electrodes were provided by means of an ultrasonic wedge bonder. Finally, the electrical contacts were encapsulated with silicone rubber.

2.3. Measurement set-up

For experiments, the PCB substrate with the combined dissolved H_2 sensor was mounted into a home-made measuring cell as it is schematically shown in Fig. 1. The front side of the sensor chip was contacted by the electrolyte and a conventional liquid-junction Ag/AgCl reference electrode (Metrohm). The sidewalls of the combined sensor chip were protected from the electrolyte solution by means of an O-ring, thereby circumventing the need for a complicated encapsulation process. The contact area of the combined sensor with the solution was about 0.4 cm^2 in total. Since the response of the field-effect pH sensor is inversely proportional to the buffer capacity [37], the measurements were performed in a low-capacity buffer solution to obtain a high sensor signal. As electrolyte, a 0.25 mM polymix multi-component buffer solution (pH 7) containing 100 mM sodium chloride (NaCl) as an ionic-strength adjuster was used [38,39].

The test chamber was provided with a gas inlet and outlet. Hydrogen gas was dissolved in the electrolyte through a perforated tube. The required gas composition was obtained by mixing hydrogen and nitrogen in various ratios (from 0 to 3% (v/v), H_2) using commercial mass flow controllers (El-Flow, Bronkhorst High-Tech). The experiments were performed in a dark Faraday cage at room temperature (ca. 22°C) and at a gas flow rate of 100 sccm.

The combined sensor has been characterized by means of amperometry using a potentiostat (PalmSens handheld potentiostat/galvanostat), and constant-capacitance (ConCap) method using an impedance analyzer (IM6, Zahner Elektrik). For the amperometric detection of dissolved H_2 , a standard two-electrode configuration under potential control was used. The potential was set at +0.55 V vs. the Ag/AgCl reference electrode and the hydrogen concentration-dependent current was sampled every second. The ConCap mode allows a dynamic characterization of the field-effect EIS sensor. In this mode, the capacitance of the EIS sensor is kept constant (usually within the depletion region of the capacitance–voltage curve at ~60% of the maximum capacitance) using a feedback-control circuit, and potential changes at the transducer/electrolyte interface were directly monitored. For operation of the field-effect sensor, a DC (direct current) polarization voltage is applied via the reference electrode to set the working point of the EIS sensor, and a small AC (alternating current) voltage (20 mV) is applied to the system in order to measure the capacitance of the sensor. All field-effect measurements were carried out at a frequency of 120 Hz. A custom-made LabVIEW “virtual instrument” program (except ‘program’ in computers) was developed for experimental control and data acquisition.

3. Results and discussion

3.1. pH sensitivity of the capacitive EIS sensor

Before the H_2 experiments were performed, the pH sensitivity of the capacitive field-effect p-Si–SiO₂–Ta₂O₅ structure has been characterized. Fig. 3 depicts a typical dynamic ConCap response of the EIS sensor recorded in Titrissol buffer solution with different pH values. The EIS sensor shows an average pH sensitivity of 57.4 mV/pH in the linear range from pH 3 to 9, which is in good agreement with pH sensitivity values reported in literature for a Ta₂O₅ layer [34,40,41].

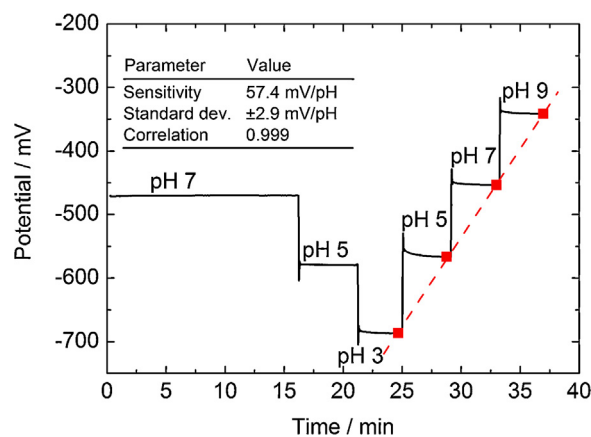


Fig. 3. Typical dynamic ConCap response of a capacitive p-Si–SiO₂–Ta₂O₅ field-effect EIS structure recorded in Titrissol buffer with different pH values from pH 3 to pH 9 and corresponding calibration curve (inlet).

3.2. Validation of independent functioning of the one-chip integrated field-effect and amperometric transducers

The functioning principle of the pH-sensitive field-effect sensor is based on the detection of pH-induced potential changes at the gate-insulator/electrolyte interface, whereas the amperometric detection relies on an electron-transfer reaction (reduction or oxidation) of an electro-active specimen at the working electrode. Since the developed dissolved H_2 sensor combines both transducer principles, in separate experiments, the independent functioning of the field-effect and amperometric transducers integrated on one single chip has been investigated. For this, HCl was added to the measuring solution to stimulate a response of the field-effect sensor and simultaneously, to study the impact of pH changes on the amperometric signal. On the other hand, the well-known electrochemically reversible ferri-cyanide/ferrocyanide ($[\text{Fe}(\text{CN})_6]^{3-}/[\text{Fe}(\text{CN})_6]^{4-}$) redox couple was used to clarify whether the signal of the field-effect transducer is affected by the electron-transfer reactions (without the proton generation) at the amperometric transducer or not. The results of these experiments are summarized in Fig. 4. Here, the time-dependent responses of the combined amperometric/field-effect sensor simultaneously recorded at different measuring conditions are depicted. The working electrode of the amperometric transducer was

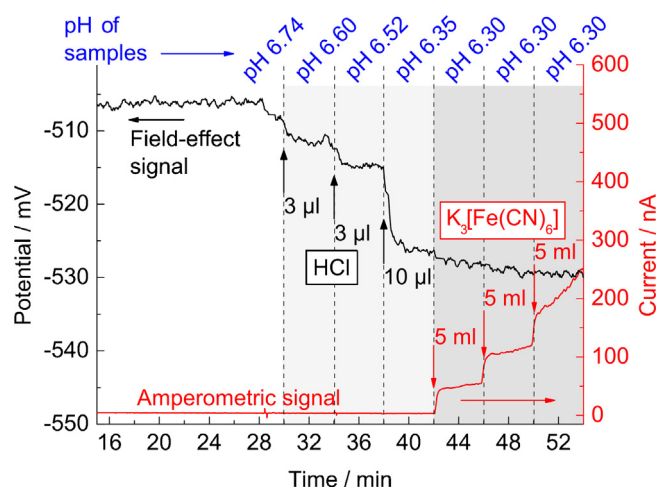


Fig. 4. Validation of independent functioning of the one-chip integrated field-effect and amperometric transducers. The pH value of samples was controlled with a conventional pH-glass electrode, simultaneously.

polarized at a potential of +0.4 V vs. the Ag/AgCl reference electrode related to the reduction of $[\text{Fe}(\text{CN})_6]^{3-}$. A phosphate buffer (0.1 mM, pH 7) adjusted with 100 mM NaCl was used as electrolyte solution and stirred continuously. The pH value of the electrolyte solution was monitored in addition with a conventional pH-glass electrode (Metrohm).

During the start-up period of the experiment (initial 30 min), both transducers show a stable response behaviour in phosphate buffer. After 30 min, 3 μL HCl was added to the electrolyte and the titration with HCl was repeated twice with titration volumes of 3 μL (34 min) and 10 μL (38 min) HCl. A total potential shift of 22 mV towards more negative potential values was observed for the field-effect device, which corresponds to a pH decrease of $\Delta\text{pH} \sim 0.4$. An additional analysis with a pH-glass electrode of samples drawn before and after each titration step confirmed this pH shift (see Fig. 4). On the contrary, the amperometric transducer shows a stable signal throughout this first part of the experiment and is therefore, not affected by the pH change of the solution.

In the next step, 5 ml of potassium hexacyanoferrate(III) ($\text{K}_3[\text{Fe}(\text{CN})_6]$) was added to the solution (42 min, 46 min, 50 min) to stimulate redox reactions at the Pt working electrode. As expected, the amperometric transducer responds immediately with an increase of the current of about 45 nA after each addition of $\text{K}_3[\text{Fe}(\text{CN})_6]$. At the same time, the field-effect sensor signal remains practically stable (some small changes in the ConCap response could be attributed to an intrinsic drift of the field-effect sensor), and thus, was not influenced by the current of the amperometric sensor. The results presented in Fig. 4 not only underline the functioning of the one-chip integrated field-effect and amperometric transducers, but also verify their independent functioning that is essential for further experiments on dissolved H_2 detection with the combined sensor chip.

3.3. Detection of dissolved H_2 with the combined amperometric/field-effect sensor

Fig. 5a demonstrates an example of a simultaneous amperometric/field-effect detection of dissolved H_2 in the concentration range from 0.05 to 3% (v/v) H_2 . The data were collected by exposing the combined sensor chip to the electrolyte with different concentrations of dissolved H_2 for 10 min. Prior to the introduction of a new hydrogen gas mixture, the electrolyte was flushed with nitrogen in order to remove the residual content of dissolved H_2 .

The amperometric sensor responded instantaneously to the H_2 dosage with a H_2 concentration-dependent increase of the output current. At the same time, the ConCap signal of the pH-sensitive field-effect sensor shifted towards more negative potentials in response to an increasing hydrogen concentration. The negative signal shift in the ConCap mode corresponds to more positive gate-surface charges as a consequence of proton generation (see Eq. (1)) at the Pt electrode. The resulting H_2 concentration-dependent local pH decrease near the surface of the pH-sensitive layer modulates the flatband voltage and output signal of the field-effect EIS sensor. For instance, with the 1% (v/v) H_2 dosage, the output signal of the field-effect sensor shifts about 13.5 ± 0.1 mV. Taking into account that the pH sensitivity of the Ta_2O_5 -gate EIS sensor is about 57 mV/pH, this signal shift corresponds to a local pH change near the surface of the pH-sensitive layer of $\Delta\text{pH} \sim 0.25$.

As can be seen from Fig. 5a, with ascending and descending H_2 dosages, a good correlation between the ConCap response of the field-effect sensor and the output signal of the amperometric sensor has been observed. The respective calibration curves of the sensors evaluated from Fig. 5a are presented in Fig. 5b. Both the amperometric and the field-effect transducer show a linear response in the H_2 concentration range from 0.1 to 3% (v/v) with a

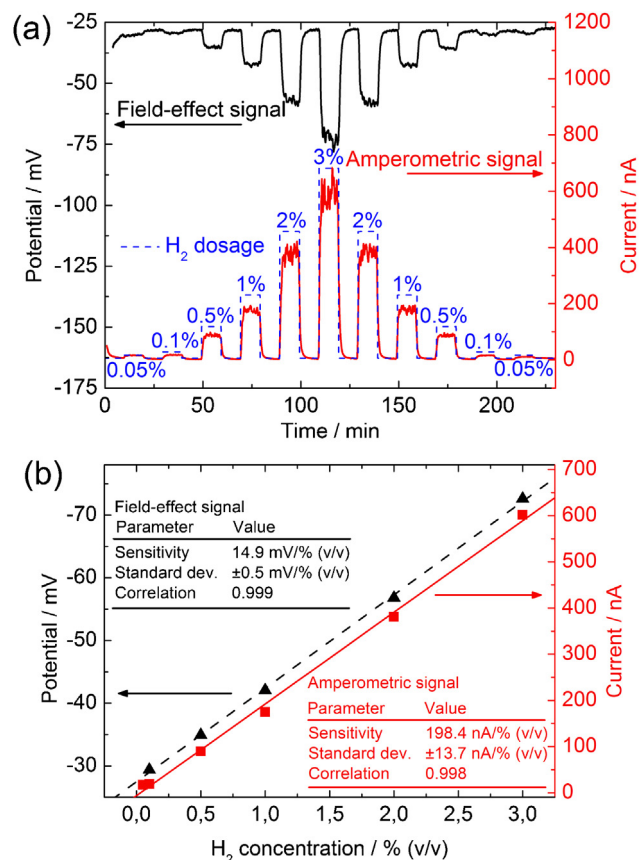


Fig. 5. Simultaneous amperometric/field-effect detection of dissolved H_2 in the concentration range from 0.05 to 3% (v/v) H_2 (a) and calibration curves of both the amperometric and the field-effect transducer, respectively (b).

H_2 sensitivity of 198.4 ± 13.7 nA/% (v/v) and 14.9 ± 0.5 mV/% (v/v), respectively. The lower detection limit has been estimated to be about 0.05% (v/v) and 0.1% (v/v) for the amperometric and field-effect sensor, respectively. Both transducers displayed practically no hysteresis (less than 2 nA for the amperometric transducer and ~ 0.35 mV for the field-effect device). The noticeable increase of noise in the amperometric sensor signal at high H_2 concentrations might be probably due to the rather random flow conditions at the Pt working electrode during the H_2 gassing.

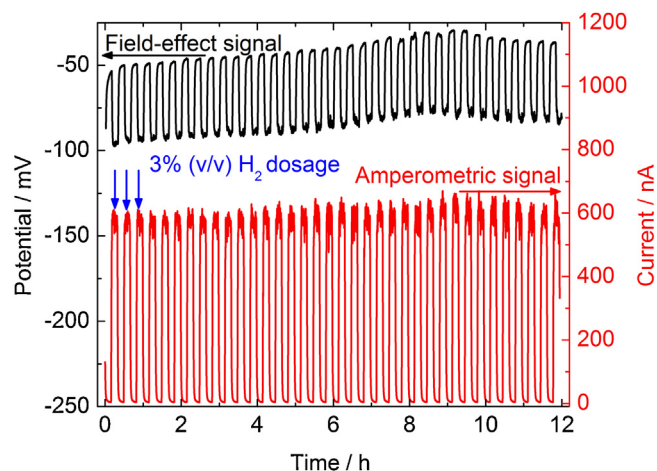


Fig. 6. Amperometric and field-effect responses of the combined sensor chip to 3% (v/v) H_2 dosage over a substantial number of measuring cycles (36 cycles).

Fig. 6 shows the amperometric and field-effect responses of the combined sensor chip to 3% (v/v) H_2 dosage over a substantial number of measuring cycles (36 cycles). Almost identical maximum output currents of approximately 580 nA were observed for the amperometric sensor over the whole measuring period, showing the stability and reproducibility of the developed sensor. The output signal of the field-effect EIS sensor changes about 45 mV in the direction corresponding to lower pH values. Whereas the amperometric signal was very stable, a relatively small drift about 2.5 mV/h was observed for the field-effect sensor.

4. Conclusions

In the present work, a one-chip integrated combined amperometric/field-effect H_2 sensor has been developed and tested in electrolyte solutions with different contents of dissolved H_2 . Both the amperometric and the field-effect transducer show a linear response in the H_2 concentration range from 0.1 to 3% (v/v) with a slope of 198.4 nA/% (v/v) and 14.9 mV/% (v/v), respectively. With increasing or decreasing H_2 dosages, a good correlation between the ConCap response of the field-effect transducer and the output signal of the amperometric transducer has been observed.

The obtained results demonstrate the independent functioning of both transducer principles on the same chip as well as the feasibility of the presented approach for a simultaneous amperometric/field-effect detection of dissolved H_2 . Such a combination of two transducer principles, namely, the amperometric and field-effect, might allow a more accurate, selective and reliable measurement of dissolved H_2 in biogas reactors and can serve as an early warning indicator of digester failures.

To overcome possible problems related to the functioning of the combined sensor in real biogas broths, future work will be directed to a direct coupling of the sensor setup with a biogas reactor via a bypass system filled with a suitable buffer solution, which will be separated from the biogas medium by a H_2 -permeable membrane (of e.g., polytetrafluoroethylene). In this way, the selectivity, lifetime and signal-to-noise ratio of the combined sensor can be improved. Moreover, to achieve a high output signal for the field-effect pH sensor, the bypass system can be filled with an appropriate low-capacity internal buffer solution.

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